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# HW High Efficiency ClO<sub>2</sub> Delignification: Process Studies

# Pro's and Con's of Vapor Phase ClO<sub>2</sub> Delignification

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- Vapor phase delignification (VPD) with ClO<sub>2</sub> is much more efficient in terms of kappa number reduction per unit of total active chlorine consumed and yields much lower extracted kappa no.
- VPD generates more AOX and would require expensive capital equipment

# Conventional and Vapor Phase D<sub>0</sub>: Conventional Hardwood Pulps

Pro- cess	Unbl. Kappa	D <sub>0</sub> Stage		(EO) Stage	
		Kappa	$\Delta\kappa/\text{TAC}$	Kappa	$\Delta\kappa/\text{TAC}$
Conv.	11.4	6.2	2.3	4.2	3.2
	15.2	7.9	2.4	5.2	3.3
Vapor	11.4	4.2	3.5	2.3	4.4
	15.2	5.3	3.8	2.5	4.9

# Having the Pro's Without the Con's

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- The essential differences between VPD and conventional delignification are the consistency and rate of  $\text{ClO}_2$  addition
- We have done experiments to independently examine the effects of these changes

# Rate of ClO<sub>2</sub> Addn. at 3% Final Consistency, 0.2 KF Applied

<b>Addn. Time, min</b>	<b>Total Time, min</b>	<b>React- or</b>	<b>(EO) Kappa No.</b>	<b>ClO<sub>3</sub><sup>-</sup> Yield, %</b>	<b>AOX Yield, %</b>
<b>0.1</b>	<b>30</b>	<b>Quant.</b>	<b>5.2</b>	<b>n.d.</b>	<b>n.d.</b>
<b>0.1</b>	<b>30</b>	<b>Rotov.</b>	<b>5.2</b>	<b>23</b>	<b>17.5</b>
<b>30</b>	<b>30</b>	<b>Rotov.</b>	<b>5.4</b>	<b>19</b>	<b>16.7</b>
<b>30</b>	<b>60</b>	<b>Rotov.</b>	<b>5.2</b>	<b>n.d.</b>	<b>n.d.</b>

# Rate of ClO<sub>2</sub> Addn. at 20% Final Consistency, 0.2 KF Applied

<b>Addn. Time, min</b>	<b>Total Time, min</b>	<b>React- or</b>	<b>(EO) Kappa No.</b>	<b>ClO<sub>3</sub><sup>-</sup> Yield, %</b>	<b>AOX Yield, %</b>
<b>0.1</b>	<b>30</b>	<b>Bag</b>	<b>2.7</b>	<b>15</b>	<b>34</b>
<b>0.1</b>	<b>30</b>	<b>Rotov.</b>	<b>2.5</b>	<b>15</b>	<b>37</b>
<b>30</b>	<b>30</b>	<b>Rotov.</b>	<b>3.4</b>	<b>n.d.</b>	<b>n.d.</b>

# Effect of Consistency

<b>Consistency, %</b>	<b>Kappa Factor</b>	<b>Addn. Time, min</b>	<b>(EO) Kappa No.</b>	<b>ClO<sub>3</sub><sup>-</sup> Yield, %</b>	<b>AOX Yield, %</b>
<b>3</b>	<b>0.1</b>	<b>0.1</b>	<b>7.0</b>	<b>12</b>	<b>17</b>
<b>3</b>	<b>0.2</b>	<b>0.1</b>	<b>5.2</b>	<b>23</b>	<b>18</b>
<b>3</b>	<b>0.2</b>	<b>30</b>	<b>5.4</b>	<b>19</b>	<b>17</b>
<b>24</b>	<b>0.11</b>	<b>0.1</b>	<b>5.6</b>	<b>11</b>	<b>32</b>
<b>20</b>	<b>0.2</b>	<b>0.1</b>	<b>2.5</b>	<b>15</b>	<b>37</b>
<b>20</b>	<b>0.2</b>	<b>30</b>	<b>3.4</b>	<b>n.d.</b>	<b>n.d.</b>

# Conclusions

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- **Slow addition of aqueous  $\text{ClO}_2$  does not reproduce the high efficiency of VPD**
- **Addition of aqueous  $\text{ClO}_2$  to high consistency pulp reproduces both the high efficiency and high AOX generation rate of VPD**
- **The characteristics of VPD are not due to vapor phase  $\text{ClO}_2$  addition, but are rather due to the high consistency of VPD**



# HexA Removal by D<sub>0</sub> Filtrate and H<sub>2</sub>SO<sub>4</sub>, 5h at 95C, pH 2.7-3.1

<b>Unbl. Kappa</b>	<b>Acid <math>\Delta\kappa</math></b>	<b>Filtrate <math>\Delta\kappa</math></b>	<b>Acid <math>\Delta n, \text{cp.}</math></b>	<b>Filtrate <math>\Delta n, \text{cp.}</math></b>
<b>11.8</b>	<b>5.1</b>	<b>5.1</b>	<b>10.1</b>	<b>0.0</b>
<b>12.9</b>	<b>5.5</b>	<b>5.7</b>	<b>3.3</b>	<b>4.7</b>
<b>17.3</b>	<b>5.0</b>	<b>5.2</b>	<b>12.3</b>	<b>16.7</b>
<b>29.1</b>	<b>4.2</b>	<b>6.0</b>	<b>21.7</b>	<b>20.2</b>

# Bleaching After Hydrolysis With Filtrate (Af Stage)

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<b>Unbl. Kappa</b>	<b>Af Kappa</b>	<b>AfD(EO) Kappa</b>	<b>D(EO) Kappa</b>
<b>16.1</b>	<b>9.5</b>	<b>2.2</b>	<b>5.2</b>
<b>11.6</b>	<b>7.0</b>	<b>2.0</b>	<b>4.2</b>
<b>24.1</b>	<b>15.4</b>	<b>3.0</b>	<b>5.2</b>
<b>14.2</b>	<b>8.8</b>	<b>2.3</b>	<b>5.2</b>
<b>7.8</b>	<b>5.6</b>	<b>1.8</b>	<b>3.1</b>

# Seeking Practical Ways to Remove Hexeneuronic Acids (HexA)

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- Investigated effects of
  - Temperature
  - Time
  - Acid source
  - Consistency

# Temp., Time Effects in Hydrolysis of Kappa 16.7 Gum RDH Pulp

Temp., °C	Time, h	Acid Source	Final Kappa No.	Viscosity, mPa.s
90	1	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	14.7	47.7
	2	"	13.5	44.1
	5	"	12.1	34.6
95	5	"	11.2	35.1
100	2	HCOOH	11.4	39.5

**Note: All runs at 4% Consistency**

# Cons'y., Time Effects in Hydrolysis of Kappa 12.6 Gum Kraft Pulp

Cons'y., %	Time, h	Acid Source	Final Kappa No.	Viscosity, mPa.s
4	5	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	6.6	24.4
12	1	"	8.7	28.8
"	3	"	7.3	26.6
"	5	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	6.8	23.3
12	"	H <sub>2</sub> SO <sub>4</sub>	6.8	24.1
20	"	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	7.7	19.5
30	"	"	7.1	15.4

**Note: All runs at 95°C**

# Medium, Cons'y. Effects in Hydrolysis of Kappa 12.6 Gum Kraft

Cons'y., %	Acid Source	Final Kappa No.	Viscosity, mPa.s
12	D <sub>0</sub>	6.6	24.4
"	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	6.8	23.3
"	H <sub>2</sub> SO <sub>4</sub>	6.4	24.9
30	D <sub>0</sub>	6.9	16.3
"	D <sub>0</sub> +H <sub>2</sub> SO <sub>4</sub>	7.1	15.4

**Note: All runs 5 h at 95°C**

# High-Intensity Hydrolysis of Kappa 12.6 Gum Kraft Pulp

Temp., °C	Time, min	HexA Released, $\mu\text{mol/g}$	Final Kappa No.	Viscosity, mPa.s
123	15	42.5	7.4	29.1
122	60	71.1	6.1	24.4

**Note: All runs at 12% consistency, pH 3, H<sub>2</sub>SO<sub>4</sub>**

# Conclusions: Medium, Time and Temperature

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- $D_0$  filtrate,  $H_2SO_4$  and formic acid are equivalent in their abilities to decrease the kappa no. of gum kraft pulp
- Kappa number reduction is nearly complete in 5h @ 95°C, 2h @ 100°C, or 30 min @ 120°C



# Conclusions: Consistency

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- For given conditions of time, temp., & initial pH, kappa reduction is independent of consistency over the range 4-30%
- Pulp viscosity loss is greater at consistencies above 12%, but may be tolerable at 30%
- Further optimization of 30% consistency hydrolysis w.r.t. temperature and time would be desirable

# Delignification Partial Sequences Incorporating Hydrolysis

Sequence	Kappa Before D <sub>0</sub>	ClO <sub>2</sub> in D <sub>0</sub> , % o.d. pulp	Kappa After (EO)	Viscosity, mPa.s
D <sub>0</sub> (EO)	12.6	0.96	3.5	33.2
AD <sub>0</sub> (EO)	6.1	0.46	1.5	n.d.
(A/D <sub>0</sub> )(EO)	6.1	0.46	2.2	21.2

**Note: A-stage conditions were 120°C, 60 min.**

# Short Sequences Incorporating Hydrolysis

Sequence	ClO <sub>2</sub> in D <sub>0</sub> +D <sub>1</sub> , % o.d. pulp	Brightness	Viscosity, mPa.s
D <sub>0</sub> (EO)D <sub>1</sub>	1.76	84.0	>25
AD <sub>0</sub> (EO)D <sub>1</sub>	0.86	85.7	n.d.
(A/D <sub>0</sub> )(EO)D <sub>1</sub>	1.26	84.8	~18

**Note: A-stage conditions were 120°C, 60 min.**

# Full Sequences Incorporating Hydrolysis

Sequence	ClO <sub>2</sub> in D <sub>0</sub> +D <sub>1</sub> +D <sub>2</sub> , % o.d. pulp	Brightness	Viscosity, mPa.s
D <sub>0</sub> (EO)D <sub>1</sub> D <sub>2</sub>	2.16	88.4	25.1
AD <sub>0</sub> (EO)D <sub>1</sub> D <sub>2</sub>	1.26	88.7	13.3
(A/D <sub>0</sub> )(EO)D <sub>1</sub> D <sub>2</sub>	1.86	88.7	<18

**Note: A-stage conditions were 120°C, 60 min.**

# Conclusions

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- Short sequences developed to date can achieve 85 brightness with  $\text{ClO}_2$  savings of more than 50%, or 30% if the pulp is not washed between the A and  $D_0$  stages
- Full sequences developed to date can achieve 88-89 brightness with  $\text{ClO}_2$  savings of more than 40%, or 15% if the pulp is not washed between the A and  $D_0$  stages

# Conclusions (Cont'd)

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- **Further optimization of the A stage may be desirable for increased viscosity retention**